

# Frequency Domain Quasi Maximum Likelihood Identification of Low Order Aeroservoelastic Models from Flight-Test Data

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# Background and Motivation

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## Low Order Equivalent System (LOES)

- From handling qualities analysis
- Traditionally simplifying complex control law and plant
- More easily understood form
- Extend LOES to a complex model due to aeroelasticity

## Maximum likelihood (Filter Error) System Identification

$$\mathbf{Z} = \mathbf{H}_{loes}(\mathbf{U} + \mathbf{W}) + \mathbf{V}$$

- There are a lot of parameters
  - Estimate noise parameters
  - Extra outputs mean extra parameters to estimate
- Usually assume noise model to simplify
  - Output Error and Equation Error
  - Results in biased estimates of the parameters
- Sensing flexible aircraft have many outputs
  - Quasi maximum likelihood exploits redundancy of outputs

# Definition of Model

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Low order system

$$H_{loes}(s|\boldsymbol{\vartheta}) = \mathbf{C} \frac{\mathbf{S}_6 s^6 + \dots + \mathbf{S}_1 s + \mathbf{S}_0}{\prod_{j=1}^3 (s^2 + 2\zeta_j \omega_{n_j} s + \omega_{n_j}^2)} \mathbf{B}$$

6-th order transfer function

- 2<sup>nd</sup> order modes (frequency damping)
- 3 modes (pitch, bending, and torsion)
- Relative degree zero

Frequency domain ( $s=i\omega$ )

Parameters ( $\boldsymbol{\vartheta}$ )

- Natural frequency
- Damping
- Numerator coefficients
  - matrices with 3 rows
  - one for each mode

# Fitting the Model

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Low order system

$$\mathbf{H}_{loes}(s|\boldsymbol{\vartheta}) = \mathbf{C}\mathbf{H}\mathbf{B}$$

## Estimate states and output matrix ( $\mathbf{C}$ )

- Neglecting the inherent dynamics
  - Only done once
- Averaging over spatially distributed sensors
  - Asymptotically unbiased as the number of outputs is increased
  - Hence the Quasi maximum likelihood
- Reducing large number of outputs, to a small number with little sensor noise

## Estimate transfer function parameters

- Similar to output error frequency domain system identification
- Results have a different interpretation
- Details in the paper

# Estimating States and Output Matrix

## Outputs by principal factor analysis

$$\mathbf{Z} \triangleq \mathbf{V}\mathbf{S}\hat{\mathbf{X}}$$

- Generalized singular value decomposition of the data
  - Only states ( $\hat{\mathbf{X}}$ ) are complex numbers
  - Keeping 3 largest singular values
  - State correlation matrix,  $\hat{\mathbf{P}} = \mathbf{V}^{-1}\mathbf{Z}(\mathbf{V}^{-1}\mathbf{Z})^T$
- Sensor noise

$$\hat{\mathbf{\Sigma}} = \text{diag}(\mathbf{Z}\mathbf{Z}^T - \mathbf{V}\mathbf{S}\hat{\mathbf{P}}\mathbf{S}\mathbf{V}^T)$$

- Difference of the signal variance, and the variance from the decomposition
- State estimate
  - Expected value of the state given the measured output

$$\hat{\mathbf{X}} = (\mathbf{I} + \hat{\mathbf{P}}\mathbf{S}\mathbf{V}^T\hat{\mathbf{\Sigma}}^{-1}\mathbf{V}\mathbf{S})^{-1}\mathbf{S}\mathbf{V}^T\hat{\mathbf{\Sigma}}\mathbf{Z}$$

- Equivalent to Kalman filter as dynamics become infinitely fast
- Least square estimates are shrunk to correct for sensor noise

$$\hat{\mathbf{X}} = \left[ (\mathbf{S}\mathbf{V}^T\hat{\mathbf{\Sigma}}^{-1}\mathbf{V}\mathbf{S})^{-1} + \hat{\mathbf{P}} \right]^{-1} \cdot (\text{least squares})$$

## Inputs by least squares

- This is the minimum bias approach

# Flight Test Results

Case	Airspeed, kn	Fuel, lb	Flight
1	80	62	16
2	110	23	34

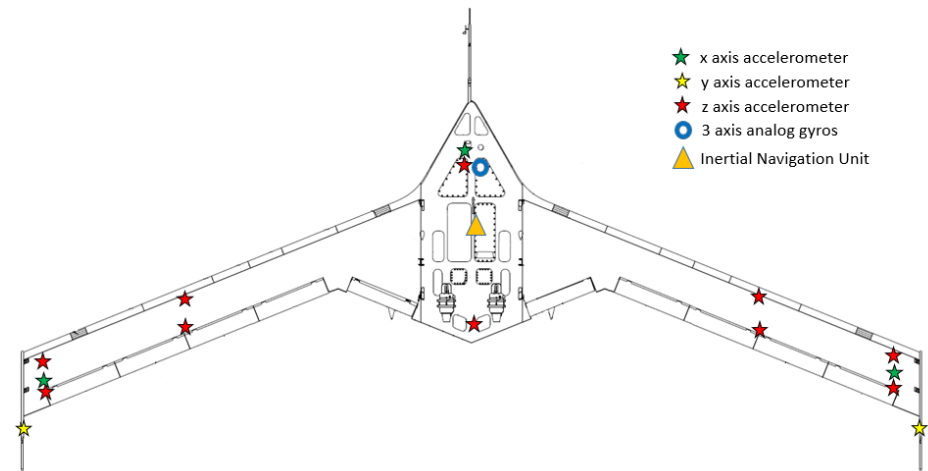


X-56A flex wing

Pitch multisines

Maneuver designed for the modes

Above and below flutter speed



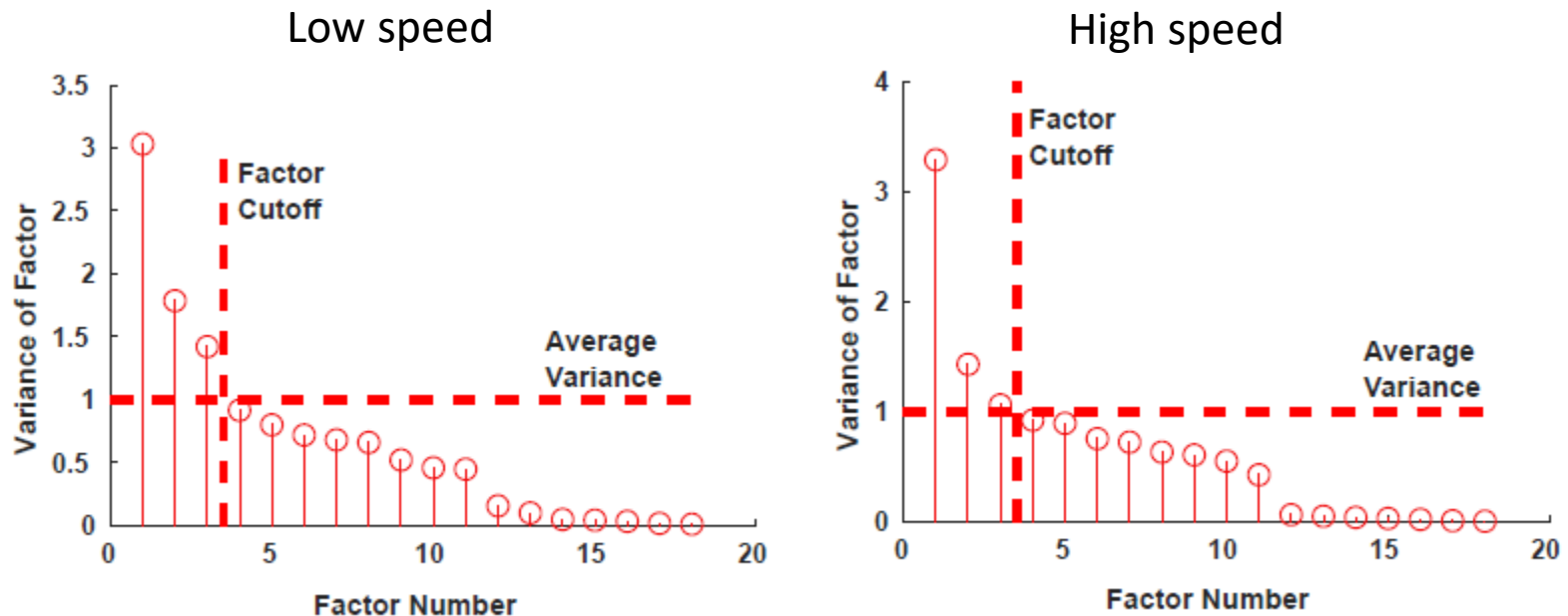
# Selecting the number of modes

Examining diagonal of singular value matrix

3 modes is a reasonable solution

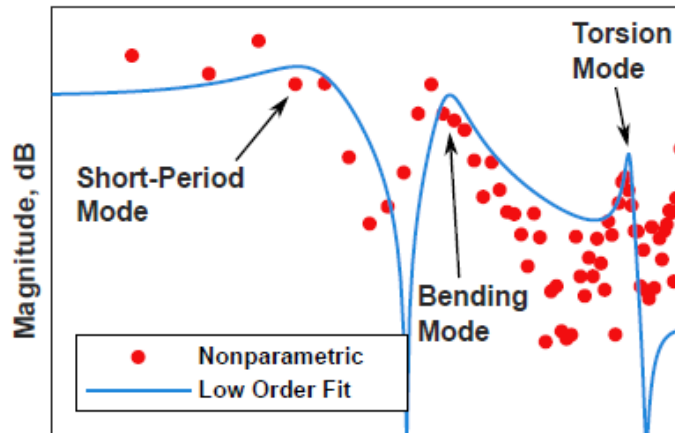
There could be as many as 11 modes

- This required more tuning of the model to flight condition

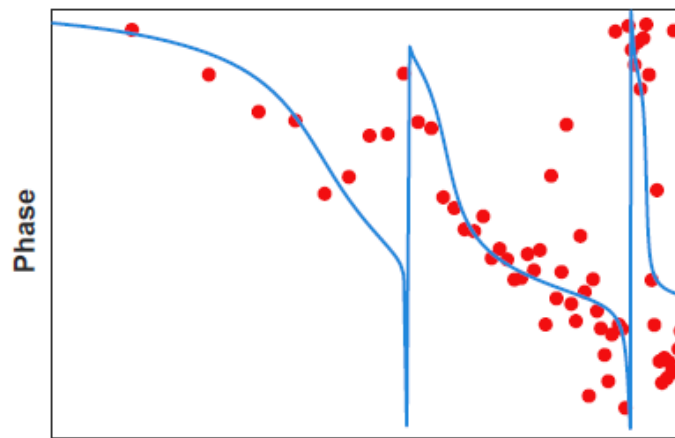
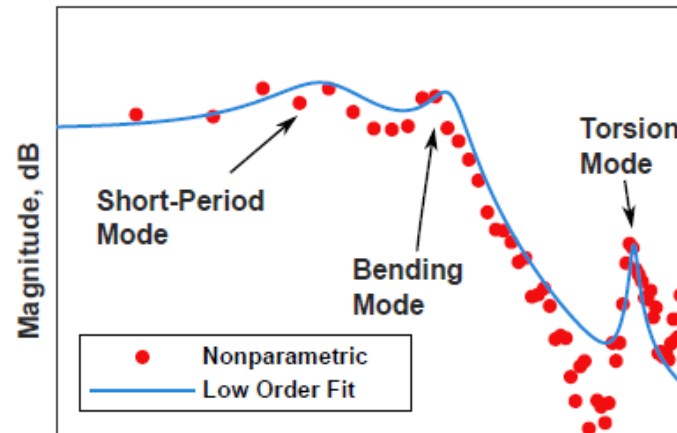


# Low speed frequency response

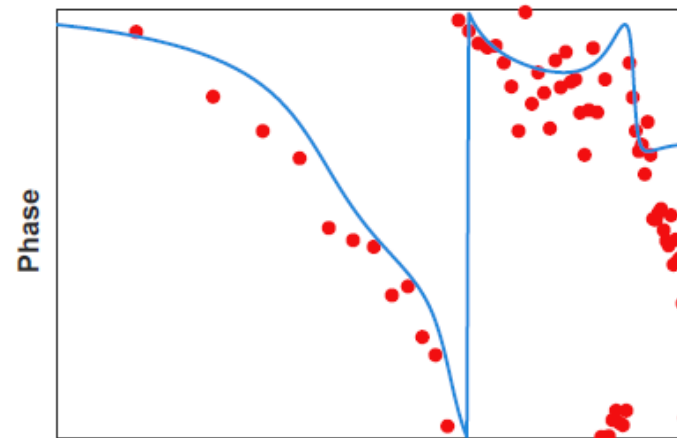
Center accelerometer



Strain gage



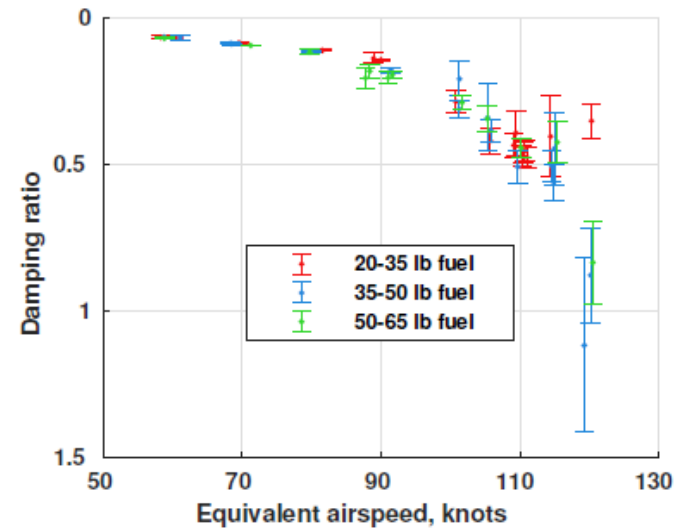
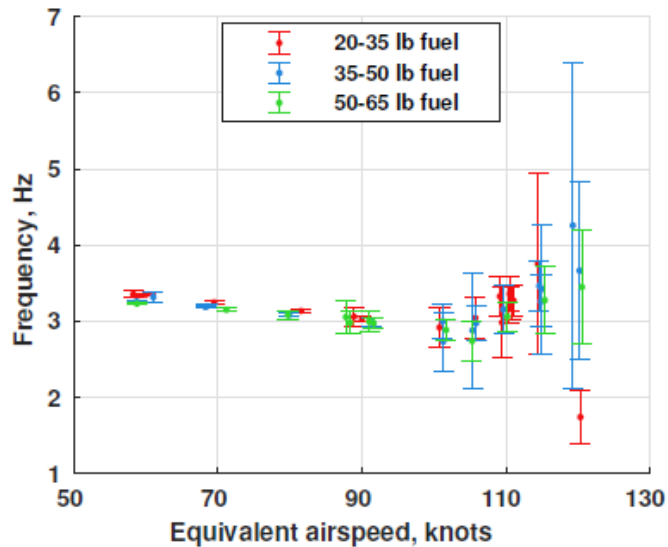
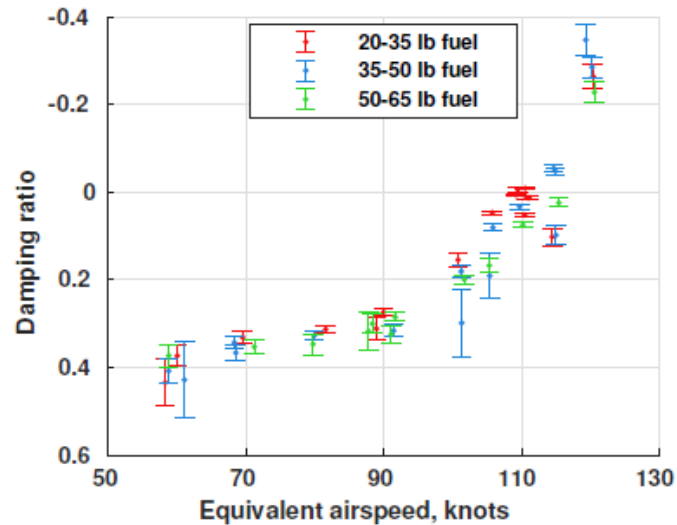
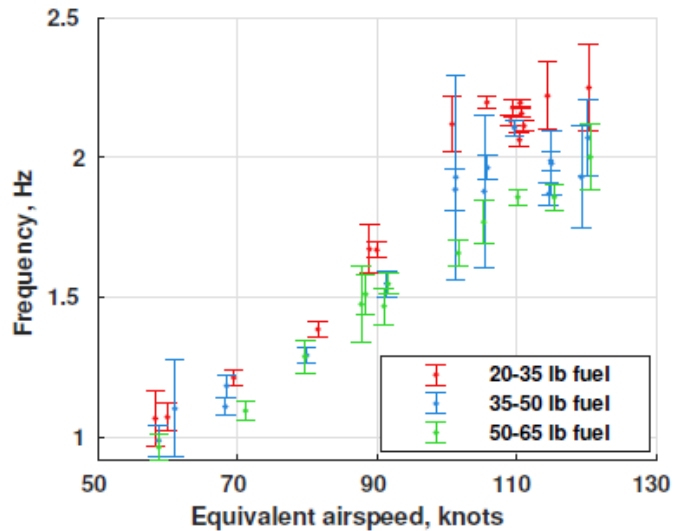
Frequency



Frequency



# Frequency and damping



# Conclusions

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## Quasi maximum likelihood estimate of low order system

- Using large number of sensors to “average” out noise
- Consistent with full maximum likelihood as number of measurements is increased

## Frequency-domain system identification

- Worked very well for open loop unstable aircraft

## Method was reliable

- A single model structure was fit to most flight conditions without readjustments